## VERIFICATION OF A TRANSLATION

I, the below named translator, hereby declare that:

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I am knowledgeable in the English language and in the language in which the below identified international application was filed, and I believe the English translation of the international application No. PCT/EP00/07550 is a true and complete translation of the above identified international application as filed.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application of any patent issued thereon.

Alum Williams (translator)

## EP-85015/PCT

## Device for extruding plastic compounds

The invention relates to a device for extruding plastic compounds having the features mentioned in the precharacterising clause of Claim 1.

- Bakery and confectionery products are often produced by

  5 extruding a plastic dough compound or sugar/fat compound.

  In this case, the pressurised compound is extruded through
  a die to form an extrudate. The extrudate itself may be cut
  and/or removed by a conveyor belt. The external form of the
  extrudate depends on the shape of the die and, in

  10 particular, on the exit velocity of the compound from the
  - oparticular, on the exit velocity of the compound from the die. If the exit velocity of the compound fluctuates, then the cut extrudate sections will differ in length, or the extrudate on the conveyor belt removing it will be formed with a non-uniform thickness.
- DE-A-44 33 593 discloses a process for controlling an extruder for foodstuffs, in which a viscosity sensor, which determines measured variables such as the product temperature, the pressure in front of the die, the specific mechanical energy input, in particular the viscous
- 20 properties, and optionally also the dwelling time, is installed between a worm tip and a die. The aim of the process is to optimise and stabilise the working point of the extruder. To that end, the rotational speed, the mass flow rate and the water content are mentioned as
- 25 manipulated variables. In order to find the optimum working point, functional relationships between the manipulated variables and product criteria, such as colour, solubility or degree of expansion, are firstly determined by running various configurations on the extruder. Three further
- 30 control stages are subsequently carried out by using the measured variables of the viscosity sensor.

WO 89/04610 discloses a process and an installation for making dough, in which a whirling mixer intimately mixes dry components with water and sends them in free fall directly to a kneading device. The kneading device delivers shaped crumbly dough uniformly to two press screws, the feed to the individual press screws being controlled, in each case on the basis of the motor power consumption, as a function of the pressure in a press head. In order to prevent stagnation of crumbly dough in front of the press screws, the latter have a higher delivery power than the kneading device. So that no air inclusions occur in the press screw, a vacuum space needs to be arranged between the kneading device and the press screw.

DE-A-22 15 449 and DE-A-43 14 728 each disclose a roller

press for extruding plastic compounds with two counterrotatable rollers. The rollers have delivery strips, which
revolve with the rollers and deliver the compound into a
pressure chamber. The compound is separated from the
rollers at a respective stripper and flows out of the

pressure chamber to exit dies. Such a roller press delivers
the plastic compounds in pulses, since the compound is
delivered more strongly by the delivery strips than in the
spaces between two delivery strips. The pulsating delivery
leads to a fluctuating exit velocity of the compound from

25 the exit dies.

The term "dough compound" means a mixture of different baking substances. These react with one another in the course of time, so that the dough compound can no longer be properly baked. This is referred to as "overageing" of the dough compound. A dough compound can therefore be processed only up to a certain time after mixing.

Furthermore, when a dough compound is being processed, it is important that it should not be exposed to any large shear forces. Large shear forces break the adhesion of the substances to one another, and individual substances, for example yeast cultures,

become damaged. The composition of the dough compound is therefore destroyed.

In a sugar/fat compound, large shear forces in the compound can lead to the segregation of fat. The composition of the sugar/fat compound is therefore likewise destroyed. The desired confectionery product can then no longer be produced.

It is an object of the invention to provide a device for extruding plastic compounds, in which the aforementioned 10 disadvantages are avoided.

The object is achieved according to the invention by a device having the features of Claim 1.

For the extrusion of dough or sugar/fat compounds, roller presses are used which, owing to their design, provide an oscillating delivery pressure. Furthermore, in the case of rotatable dies, an oscillating fluctuation of the flow resistance of the compound in the die also occurs. According to the invention, the two oscillating quantities are adapted to one another in such a way as to produce a substantially constant exit flow rate of the compound from the die. Alternatively, in the case of a non-rotating die, an instrument may be provided which adapts the flow resistance of the die to the fluctuating delivery pressure of the feed instrument, so that a substantially constant exit flow rate of the compound is likewise achieved.

Dough compound is an elastoviscous compound (Maxwell medium) which may be both viscous (Newtonian fluid) and elastic (elastic body). The viscous dough compound hence solidifies, for example, during baking, which is of course desired.

30 Furthermore, however, the dough compound also solidifies during the processing time. From the consistency or viscosity of the dough compound, it is therefore possible to deduce whether the dough compound can, or should, continue to be processed. By virtue of the sensing instrument of the device according to the invention, it is therefore readily possible to detect whether a dough compound in the extrusion device is "overaged". Previously, this was not detected until at a downstream oven, so that fairly large amounts of waste were produced in the meantime.

The fat contained in a sugar/fat compound is a so-called non-Newtonian substance, i.e. it does not behave as a viscous compound. If the composition of the viscous sugar/fat compound is destroyed by large shear forces, fat is separated and the viscosity of the compound hence changes. Therefore, during the processing of a sugar/fat compound, it is also possible to detect, using the sensing instrument of the device according to the invention,

According to an advantageous refinement of the device, the measured variable is the pressure of the compound. The following will be given as an explanation: for the flow of a viscous compound (Newtonian fluid) through a tube, the

15 whether the sugar/fat compound has the required composition.

 $V' = [\pi \bullet R^4 (p_1 - p_2)] : (8 \bullet \eta \bullet 1)$ 

20 following applies

where V' is the volume flow rate of the compound, R is the tube radius, p<sub>1</sub> is the pressure of the compound at the tube start, p<sub>2</sub> is the pressure of the compound at the tube end,

25 η is the dynamic viscosity (consistency) of the compound and l is the length of the tube (see Hering et al.: Physik für Ingenieure [Physics for engineers] page 122, VDI-Verlag, Düsseldorf, 1989). When rewritten, this equation becomes:

$$\eta = [\pi \bullet R^4 (p_1 - p_2)] : (8 \bullet V' \bullet 1).$$

30 Herein, R and l are constant. Furthermore,  $p_2$  corresponds to the external pressure and can likewise be regarded as constant. If it is assumed that, at least for a certain time, the feed instrument feeds a constant flow rate V'

into the tube, i.e. the die, then the pressure  $p_1$  in the compound depends directly on the viscosity  $\eta$ . If the pressure changes, then this corresponds to a change in the viscosity of the compound and therefore, for example, to overaging of the dough compound.

The friction force  $F_R$  of the compound is equal to the pressure force  $F_P$  acting at the tube ends (ibid.):

$$F_R = F_P = (p_1 - p_2) \bullet \pi \bullet R^2$$
.

This means that when the pressure p<sub>1</sub> in the compounded 10 rises, the friction force F<sub>R</sub> also increases. The pressure p<sub>1</sub> is therefore a measure of the friction force F<sub>R</sub> of the compound. The friction force F<sub>R</sub> depends on the flow resistance of the compound in the die and on the shear forces in the compound. As described above, the compound should not be exposed to large shear forces. With the aid of the determined pressure in the compound, it is then possible to limit the friction force on the compound and hence prevent its damage.

According to a further or alternative configuration of the 20 device, the measured variable is the flow rate of the compound. According to the aforementioned equation

$$\eta = [\pi \bullet R^4 (p_1 - p_2)] : (8 \bullet V' \bullet 1),$$

the viscosity  $\eta$  depends on the pressure  $p_1$  and the volume flow rate V'. Through suitable means which limit the 25 pressure  $p_1$ , it is possible to keep constant the pressure  $p_1$  prevailing in the die. The viscosity  $\eta$  therefore depends only on the volume flow rate V' of the compound. The volume flow rate V' of an incompressible fluid through a tube is

$$V' = \pi \bullet R^2 \bullet V_m$$

where  $v_m$  is the average flow rate, or the exit flow velocity, of the compound. Determining the flow rate of the compound hence makes it possible to determine both the emerging volume flow rate and any change in the viscosity of the compound.

According to an advantageous configuration of the invention, the sensing instrument is coupled to a control instrument, and the control instrument is capable of controlling the feed instrument, as a function of at least one measured value determined by the sensing instrument, in such a way that the exit velocity of the compound from the die is not only substantially constant, but fluctuates minimally. The effect of a uniform exit velocity of the compound is that the bakery or confectionery products which are produced have a uniform shape and weight.

According to the above equations, the following applies:

$$V' = \pi \bullet R^2 \bullet v_m = [\pi \bullet R^4 (p_1 - p_2)] : (8 \bullet \eta \bullet 1).$$

The average flow rate or exit velocity  $v_m$  can therefore be adapted by appropriately adapting the volume flow rate V' 20 or the pressure  $p_1$  in the die by using the feed instrument.

According to an advantageous configuration of the device according to the invention, it comprises a transport instrument for removing the compound extruded from the die, the sensing instrument being coupled to the control instrument, and the control instrument being capable of controlling the transport instrument, as a function of at least one measured value determined by the sensing instrument, in such a way that the transport velocity of the transport instrument corresponds to the exit velocity of the compound from the die.

In the known devices, the transport velocity of the transport instrument is constant, so that a non-uniformly

emerging compound, when arriving on the transport instrument, is stretched or compressed by the latter. According to the invention, the exit velocity of the compound and its removal rate are equal, so that a uniformly shaped compound extrudate is obtained.

According to a further advantageous configuration of the invention, the device comprises a rotary instrument having at least one rotatable die, the sensing instrument is operatively coupled to the control instrument, and the control instrument is capable of controlling the rotary instrument, as a function of at least one measured value determined by the sensing instrument, in such a way that the exit velocity of the compound from the die fluctuates minimally.

15 In the case of a rotatable die, the flow resistance of the die generally fluctuates during the rotation. The friction force  $F_R$  of the compound therefore changes. According to the above equations, however, it is possible to adapt the flow rate  $v_m$  of the compound as desired, by appropriately 20 adapting the pressure  $p_1$  in the compound by means of the feed instrument. This can be done, according to the invention, by using a control instrument.

In order to obtain bakery products with a plurality of extrudates, a feed instrument is connected through a plurality of channels to a die having a plurality of outlet openings, and a sensing instrument is in each case arranged at the channels or the outlet openings of the die.

The latter device is advantageously adjusted in the following way: the sensing instruments are operatively

30 coupled to the control instrument, and the control instrument is capable of controlling the feed instrument, as a function of the measured values determined by the sensing instruments, in such a way that the exit velocities of the individual compounds from the outlet openings of the die fluctuate minimally relative to one another. By virtue of such uniformly emerging compounds, the layering of the

bakery or confectionery products which are made has a constant thickness. The products therefore have an especially high level of dimensional and weight accuracy.

By using the device according to the invention, it is hence 5 possible to make bakery or confectionery products with a much higher level of weight and shape accuracy than is the case with known devices.

The appended schematic drawing shows an exemplary embodiment of the device according to the invention for 10 extruding plastic compounds, which will be explained in more detail below.

A device 10 for extruding plastic compounds comprises a feed instrument 12, which is configured as a roller press and by means of which compounds, for example dough or sugar/fat compounds, can be fed to a die 14. A transport device 16 in the form of a conveyor belt is arranged below the die 14. The emerging compounds pass, shaped into an extrudate, onto the transport instrument 16 and are removed horizontally by it. Bakery products are formed, for example, which are baked in a downstream oven (not shown).

The extrudate may be cut or sealed by a cutting or pinching device (not shown), so that the cut sections of the extrudate are removed on the transport instrument 16.

Furthermore, a plurality of dies 14 may be arranged next to one another, so that the capacity of the device is correspondingly enhanced.

For delivering and feeding the compounds, the feed instrument 12 has three pairs of rollers 18a, 20a, 18b, 20b and 18c and 20c which, in a manner which is known and is 30 therefore not described in detail here, receive the compounds from a respective supply line 22a, 22b and 22c. The rollers 18a to 18c and 20a to 20c have, distributed at the circumference, delivery strips which each deliver one compound into a respective pressure space (not shown).

During this, the delivery pressure generated by the delivery strips fluctuates according to the position of the delivery strips in the pressure space. The feed instrument therefore generates an oscillating delivery pressure which, in particular, fluctuates with the delivery rate  $v_a,\ v_b$  and  $v_c$  of the individual pairs of rollers.

When the rollers turn, the compounds are delivered with the feed pressure into channels 24a, 24b and 24c, respectively. The compounds reach the die 14, which is designed as a 10 triple die and has three outlet openings (not shown). The outlet openings are arranged in such a way that the emerging compound forms an extrudate (not shown). The die 14 can be rotated with a rotational velocity  $v_d$  by means of a rotary instrument 26. The die 14 has 15 asymmetrically arranged connection and ring channels (not shown) so that the compounds can flow from the channels 24a to 24c to the outlet openings even when the die 14 is turning. When the die 14 turns, differing flows pass through the individual connection and ring channels, so 20 that the flow resistance of the compounds therefore fluctuates, and in particular this fluctuation oscillates as a function of the rotational velocity  $v_d$  of the die 14.

The rollers 18a to 18c and 20a to 20c can each be driven by a feed drive, these being operated by separately ventilated 25 electric motors 28a, 28b and 28c, respectively. In this case, a respective temperature sensor 30a, 30b and 30c and hand switch 32a, 32b and 32c for manual operation is arranged at each of the electric motors 28a to 28c. The electrical supplies of the electric motors 28a to 28c are 30 each provided with a respective frequency converter 34a, 34b and 34c and speed regulator 36a, 36b and 36c, by means of which it is possible to vary the rotational speed of the electric motors 28a to 28c and therefore the delivery rates Va. Vb and Vc.

35 The rotary device 26 has a rotary drive, which can be driven by means of an electric motor 38. A temperature sensor 40 and a hand switch 42 are provided at the electric motor 38. The

rotational velocity  $v_d$  of the electric motor 38 can be adapted by means of a frequency converter 44 and a speed regulator 46.

The transport instrument 16 comprises a transport drive,

which can be driven by means of an electric motor 48 with a
separately driven fan (not shown), a temperature sensor 50
and a hand switch 52. To regulate the rotational speed of
the electric motor 48, and therefore a transport rate v<sub>t</sub> of
the conveyor belt, the electric motor 48 has an encoder 54,

a frequency converter 56 and a speed regulator 58.

A pressure sensor 60a, 60b and 60c, respectively, is in each case arranged at the channels 24a to 24c, and, as a sensing device, is capable of determining the pressure  $p_a$ ,  $p_b$  or  $p_c$  of the extruded compounds which prevails in the 15 respective channels 24a to 24c.

The frequency converters 34a, 34b and 34c, 44 and 56, as well as the pressure sensors 60a, 60b and 60c are operatively coupled through lines (only partially shown) to a control instrument 62. The control instrument 62 is configured as a programmable logic circuit and can change the delivery or feed rates  $v_a$ ,  $v_b$  and  $v_c$  of the feed instrument 12, the rotational velocity  $v_d$  of the rotary instrument 26 and the transport rate  $v_t$  of the transport instrument 16 by means of the frequency converters 34a to 34c, 44 and 56, respectively.

In this case, the pressures  $p_a$ ,  $p_b$  and  $p_c$  determined by the pressure sensors 60a to 60c are processed by the control instrument 62.

According to a first control method, the control instrument 30 62 in this case adapts the feed rates  $v_a$ ,  $v_b$  and  $v_c$  in such a way that the pressures  $p_a$ ,  $p_b$  and  $p_c$  are constant, so that, if the viscosity of the compounds remains the same, their exit velocity fluctuates minimally.

A second control method is configured in such a way that 35 the transport rate  $v_t$  is adjusted to the exit velocity  $v_s$  of

the emerging extrudate, so that the extrudate is not stretched or compressed when it arrives on the conveyor belt.

According to a third control method, the rotational velocity  $v_d$  is adapted to the delivery rate  $v_a$  to  $v_c$ , so that the fluctuating delivery pressure of the feed instrument 12 and the fluctuating flow resistance of the die 14 compensate for one another. For the revolution of n delivery strips of a roller during the time t, the rotational velocity  $v_d$  is selected in such a way that the

0 rotational velocity  $v_d$  is selected in such a way that the die 14 rotates n times or with a multiple of n.

In a fourth control method, the delivery rates  $v_a$  to  $v_c$  are matched to one another in such a way that, depending on the viscosity of the individual compounds, pressures  $p_a$ ,  $p_b$  and  $p_c$  prevail in the individual channels 24a to 24c such that the exit velocities of the compounds fluctuate only minimally relative to one another.

Alternatively, the pressure sensors 60a to 60c may be configured as flowmeters, the aforementioned control
20 methods being appropriately adapted to the measured variable consisting of the flow rate, so that analogous control results are obtained.